Fabrication and Characterization of α-Fe₂O₃ Nanoparticles Dispersed Epoxy Nanocomposites

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Received: April 09, 2021, Revised: June 02, 2021, Accepted: June 06, 2021, Available Online: June 21, 2021

ABSTRACT

In this work, epoxy resin matrix based polymer nanocomposites were fabricated incorporating sol-gel synthesized hematite (α -Fe₂O₃) nanoparticles. The effect of nanoparticles on chemical, mechanical, electrical, optical and thermal properties in polymer matrix was evaluated. Different functional groups were present in α -Fe₂O₃ nanoparticles, neat epoxy and α -Fe₂O₃/epoxy nanocomposites that obtained from Fourier-Transform Infrared spectroscopy (FTIR). Vibrating Sample Magnetometer (VSM) analysis revealed that the α -Fe₂O₃ nanoparticles have superparamagnetic character. By incorporation of nanoparticles into the epoxy matrix decreased the tensile strength and elongation at break, and increased Young's modulus. In addition, the addition of nanoparticles into the epoxy matrix gradually reduced and increased of the flexural strength and hardness, respectively. The improvement in light absorbance of α -Fe₂O₃/epoxy nanocomposites was increased with increasing the α -Fe₂O₃ content. Conversely, the optical band gap was decreased with increasing nanoparticle addition.

Keywords: α-Fe₂O₃ Nanoparticles, Nanocomposites, Mechanical Properties, Epoxy Resin, Thermogravimetric Analysis (TGA).



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1 Introduction

Organic-inorganic nanohybrid materials have been widely studied because of their unique properties resulting from the combination of both organic polymer and inorganic nanoparticles [1]-[8]. Also, there has been strong emphasis on the advancement of polymer nanohybrids, in which at least one of the dimensions of the filler has nanometer scale. Researchers have long known that decreasing filler dimension increases the specific surface area of the filler, which in turn may effectively improve the transfer of the load between the polymer matrix and fillers. These nanohybrid materials may exhibit significant enhancements in thermal, mechanical, and electrical properties that are difficult to achieve using conventional fillers with micro scale dimensions, such as carbon, glass, or aramid fibres. In order to reduce the gap between the performances of today's engineering polymers and the ever-increasing demand of engineering applications, new nanohybrids are needed with optimum nanofillers dispersion, improved load transfer-ability from polymer to filler particles, and enhanced thermal properties. Generally, the reinforcement of nano-particles into the polymer matrix enhances the mechanical, dimensional, and thermal stability of the host polymer matrix.

Hematite (α -Fe₂O₃) nanoparticle is an inorganic nanofiller, exhibits some excellent properties like- low cost, environmentally friendly, low toxicity, corrosion and chemically resistance, biocompatibility, and good substrate adherence [7],[8]. Because of these excellent properties, α -Fe₂O₃ nanoparticles are used in water treatment [9], contrast reagents/drug delivery [10], sensor technology [11],[12], optical coatings, magnetic storage [13], field-effect transistors [14], catalysts [15], pigments [16],

etc. α-Fe₂O₃ nanoparticles can be synthesized by several methods, for instance, chemical vapour deposition, hydrothermal synthesis [17], sonochemical technique, chemical precipitation [18], sol-gel technique [19], microemulsion technique [20], hydrolysis [21], ball milling [22], laser ablation, sputtering, and spray pyrolysis [23]. In the past decades until now, there have been numerous investigations of different magnetic nanoparticle-based polymer nanocomposites [24]-[30]. A few examples are mentioned here. In 2008, Dusko Dudic et al. studied the electrical properties of a composite comprising epoxy resin and α -Fe₂O₃ nanorods [24]. In 2017, Prasanna B P et al. synthesized polyaniline/a-Fe₂O₃ nanocomposite electrode material for super-capacitor applications [25]. In 2016, Ali Mirzaei et al. synthesized and characterized mesoporous α -Fe₂O₃ nanoparticles to investigate the electrical properties of fabricated thick films [26].

On the other hand, epoxy resin is a thermosetting polymer with some excellent properties e.g. light weight, chemically resistance, oil and fuel resistance, electrical insulator, etc. Because of these features epoxy can be used in LEDs, printed circuit boards, inductors, marine applications, coatings, structural adhesives, electrical insulators, and other electrical, electronics, and industrial applications [27]. In 2011, Richard Voo et al. studied different properties of epoxy nanocomposite films [28]. In 2016, A. Kanapitsas et al. studied the dielectric, magnetic, and hydration behaviour of barium ferrite/epoxy nanocomposites [29]. In 2016, Masoomeh Gazderazi et al. studied the mechanical and thermal properties of hybridizing MWCNT with nano metal oxides and TiO₂ in epoxy composite [30]. The incorporation of nanofillers into the polymer matrix not

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only improves the mechanical properties, besides it also helps to extend the application of fabricated nanocomposite [31],[34].

According to previous reports, most work in this field has been done to fabricate α -Fe₂O₃ nanocomposites or Epoxy composites individually. Also, less importance was given to evaluate the mechanical, thermal, and optical properties of α -Fe₂O₃/epoxy nanocomposites. Therefore, the main objective of this work is to synthesized α -Fe₂O₃ nanoparticles which are further dispersed into the epoxy matrix to improve the mechanical and thermal properties as well as optical and electrical properties of α -Fe₂O₃/epoxy nanocomposites.

In the present study, nanocomposites containing epoxy and α -Fe₂O₃ nanoparticles with various compositions were fabricated by solution casting method on flat glass mold. The samples were characterized by various experimental techniques, and the influence of α -Fe₂O₃ nanoparticles on the mechanical, thermal, optical, and electrical properties of α -Fe₂O₃/epoxy nanocomposites was investigated.

2 Experimental Details

2.1 Materials

All the chemical reagents were of analytical grade and used without further purification. Anhydrous ferric nitrate (Fe(NO₃)₃), Anhydrous citric acid (C₆H₈O₇) were purchased from Merck (India) with a purity \geq 98 %, whereas epoxy resin and diethylene triamine (DETA) hardener were purchased from Sigma-Aldrich (India).

2.2 Synthesis of α-Fe₂O₃ Nanoparticles

Hematite (α -Fe₂O₃) nanoparticles were chemically synthesized by sol-gel process, where 200 mL (0.1M) of anhydrous ferric nitrate, Fe(NO₃)₃ used as a precursor solution which gelated by using 800 mL (0.1M) of anhydrous citric acid, C₆H₈O₇ solution as ligand molecules, and singly distilled water as the solvent. Ferric nitrate solution drop-wise added to the citric acid solution with maintaining vigorous stirring by magnetic stirrer. The mixture was heated to 70 °C and continuous stirring was maintained until the gel formation. The produced gel was then dried by evaporation. After that, the dried gel was annealed at 250 °C for 1.5 hours. Finally, the powder was grinding by mortar and pestle, typically yielding 0.85gm of α -Fe₂O₃ nanoparticles.

2.3 Fabrication of α-Fe₂O₃/Epoxy Nanocomposites

In order to fabricate the nanocomposites, a certain amount of α -Fe₂O₃ nanoparticles was added into epoxy resin and mixed carefully for 15 minutes to get a uniform dispersion of the nanoparticles within the resin. After that, the curing agent diethylene triamine (DETA) was added with continuous stirring (epoxy-curing agent ratio was 10:1 by weight). Finally, the above mixture was cast into a flat glass mold and out-gassed overnight. The produced composite sheets had an approximate thickness of 2 mm. Due to their high aspect ratio and large surface area, the contents of the α -Fe₂O₃ nanoparticles in the composite were chosen to be 0.5, 1.0, 2.5, and 5.0 wt% respectively.

2.4 Characterization Techniques

2.4.1 X-Ray Diffraction (XRD)

The XRD patterns of α -Fe₂O₃ nanoparticles were obtained using a BRUKAR ADVANCE D8 Diffractometer. The diffraction patterns were measured at room temperature using Cu K α radiation ($\lambda = 1.5406$ Å) where Bragg's angles varying from 10° to 70°.

2.4.2 Scanning Electron Microscopy (SEM)

The morphologies and microstructures of α -Fe₂O₃ nanoparticles were observed using JEOLUSER 7610F Scanning Electron Microscope, which operated at 5 kV.

2.4.3 Fourier-Transform Infrared Spectroscopy (FTIR)

The presence of different functional groups in α -Fe₂O₃ nanoparticles, neat epoxy and α -Fe₂O₃/epoxy nanocomposites were observed using PERKIN-ELMER FRONTIER FTIR/MIR Spectrometer. The FTIR spectra were recorded in the 450-4000 cm⁻¹ region.

2.4.4 Vibrating Sample Magnetometer (VSM)

The magnetization-magnetic field hysteresis loops of α -Fe₂O₃ nanoparticles were measured by using *MICROSENSE EV9 Vibrating Sample Magnetometer* at room temperature.

2.4.5 Tension and Flexural testing

The tensile tests of neat epoxy and α -Fe₂O₃/epoxy nanocomposites were conducted according to ASTM D882 (2012) using a Universal Testing Machine (Hounsfield UTM 10KN, UK). The clamping length for each specimen on each jaw was 15 mm, and no extensometer was used for the tensile tests. The tests were performed at a crosshead speed of 5 mm/min. Each value reported is the average of five sample tests. The flexural strength of neat epoxy and α -Fe2O3/epoxy nanocomposites were measured using HOUNSFIELD H10KN UTM according to the standard method used for flexural properties (ASTM D790-98 2003). The speed for the flexural test was set at 5 mm/min. In addition, each value reported is the average of five sample tests.

2.4.6 Hardness Testing

The hardness of neat epoxy and α -Fe₂O₃/epoxy nanocomposites were measured using SHIMADZU HMV-2 VICKER'S Micro-Hardness Tester. The specimen was placed on a hard, horizontal glass surface. The diamond indenter was held vertically and the scale was measured with 10 seconds, after the pressure was in firm contact with the specimen. Each sample was investigated five times at a certain load with 10 s indentation time.

2.4.7 Thermogravimetric Analysis (TGA)

The TGA curves of α -Fe₂O₃ nanoparticles, neat epoxy and α -Fe₂O₃/epoxy nanocomposites were determined using EXSTAR 6000, TG/DTA 6300 Thermal Analyzer. The rate of heating was 20 °C/min and the mass of the specimen was 2-3 mg. The measurements were carried out in nitrogen atmosphere.

2.4.8 UV-Vis Spectroscopy

The optical absorption of neat epoxy and α -Fe₂O₃/epoxy nanocomposites were recorded at room temperature using SHIMADZU UV-1601 Spectrophotometer in the range of 190-1100 nm.

2.4.9 DC Resistivity

The DC resistivity of neat epoxy and α -Fe₂O₃/epoxy nanocomposites were determined using KEITHLEY 6517B Electrometer at room temperature where the applied voltages were 10, 20, 30, 40, 50 volts, respectively for every sample.



Fig. 1 XRD patterns of α-Fe₂O₃ nanoparticles



Fig. 2 SEM images of (a) α -Fe₂O₃ nanoparticles and (b) α -Fe₂O₃/Epoxy nanocomposite.

3 Results and Discussion

3.1 XRD Analysis

The XRD patterns of α -Fe₂O₃ nanoparticles produced by the sol-gel process were illustrated in Fig. 1. The XRD peaks were recorded with the 20 value varying from 10° to 70° with Cu K α radiation (λ =1.5406Å). The XRD patterns of α -Fe₂O₃ were indexed as pure hexagonal structures. The peaks were appeared at 20 values of 24.118°, 33.2432°, 35.6757°, 40.89°, 43.41°, 49.47°, 54.069°, 57.46°, 62.327°, and 64.0° and represented by the (012), (104), (110), (113), (202), (024), (116), (122), (214) and (300) crystalline structures correspond to pure α -Fe₂O₃ nanoparticles. The diffraction peaks matched with standard JCPDS card no. 87-1164 [35], indicating that the α -Fe₂O₃

nanoparticles are crystalline structures. The average crystallite sizes were calculated by using the Debye-Scherer equation:

$$D = \frac{K\lambda}{\beta \cos\theta}$$

where K is the shape factor (the typical value is 0.94), λ is the wavelength of the incident beam, β is the broadening of the diffraction line measured in radians at half of its maximum intensity (FWHM) and θ is the Bragg's angle and D is the diameter of the crystallite size [36]. The average crystallite sizes of α -Fe₂O₃ from the XRD data were found to be around 32 nm. No other peaks were observed in the calcined compound, which indicates the formation of a pure hexagonal structure of α -Fe₂O₃ nanoparticles.

3.2 SEM Analysis

The SEM images of α -Fe₂O₃ nanoparticles and α -Fe₂O₃/epoxy nanocomposites are illustrated in Fig. 2(a) and (b), with ×100,000 and ×10,000 magnification, respectively. Fig. 2(a) shows α -Fe₂O₃ nanoparticles are well defined and oriented spindle-like with small spherical shaped particles. The average crystallite size of α -Fe₂O₃ which was calculated from the SEM image was found to be around 29 nm. From Fig. 2(a), it is clear that α -Fe₂O₃ nanoparticles are mainly present as granules with small spherical-shaped particles and are well crystalline.

Due to the very tiny particle size, the number of existing atoms/molecules on the surface was increased excessively. Therefore, the agglomeration of nanoparticles was seen due to the presence of inter-particle forces such as electrostatic forces, van der waals forces.



Fig. 3 FTIR spectrum of α -Fe₂O₃ nanoparticles, neat epoxy and 2.5% α -Fe₂O₃/epoxy nanocomposite

During the synthesis and process of nanoparticles this agglomeration commonly occurs [34]. From Fig. 2(b), it is seen that the α -Fe₂O₃ nanoparticles are more or less uniformly confined in the epoxy matrix. The inclusion of nano-sized particles impart new properties compared to polymer matrix

itself. The mechanical properties of composites either positively or negatively influences by the size of nanoparticles [35].

In composite systems, it is found that the mechanical properties such as strength, rigidity and yield strength varies with the size of incorporated particles [35].

3.3 FTIR Analysis

Fig. 3 shows the FTIR spectra of α -Fe₂O₃ nanoparticles, neat epoxy, and 2.5% α -Fe₂O₃/epoxy nanocomposite. For α -Fe₂O₃ nanoparticles, the band at 3466 cm⁻¹ is assigned to the stretching vibration of water, indicating the existence of a little water absorbed on the sample. The high-frequency band at 544 cm⁻¹ refers to Fe-O deformation in the octahedral and tetrahedral sites which gives evidence for the formation of α -Fe₂O₃.

There is no peak at 2900 cm⁻¹ indicating the C-H stretching band, which means all organic compounds are removed from the samples after calcination at 250 °C. For neat epoxy, the O-H, C-H, C=O, C=C, C=N, and C-O stretching vibration peaks are located at 3370, 2926, 1748, 1510, 1238, and 1037 cm⁻¹, respectively. The C-H bending vibration peak is located at 1366 cm⁻¹. For 2.5% α -Fe₂O₃/epoxy nanocomposite, the O-H, C-H, C=O, C=C, C-N, and C-O stretching vibration peaks are located at 3328, 2933, 1749, 1509, 1234, and 1039 cm⁻¹, respectively. The C-H bending vibration peak is located at 1371 cm⁻¹.



Fig. 4 Magnetization-magnetic field hysteresis curve of α -Fe₂O₃ nanoparticles.

3.4 VSM Analysis

The magnetic properties of α -Fe₂O₃ nanoparticles were measured by a vibrating sample magnetometer. Fig. 4 illustrates the magnetic hysteresis curve of α -Fe₂O₃ nanoparticles recorded at room temperature. It exhibits superparamagnetic behavior due to nanoscale particle size. The saturation magnetization (M_s), coercivity (H_c), and remnant magnetization (M_r) of α -Fe₂O₃ nanoparticles were 337.137×10⁻³ emu, 33.312 Oe, and 28.90×10⁻³ emu, respectively. It should be mentioned that the magnetic properties of the materials depend on the particle's size, shape, magnetization direction, crystallinity, etc.

3.5 Tensile Properties Analysis

Fig. 5 represents the stress-strain curves of neat epoxy, 0.5, 1.0, 2.5, and 5.0 wt% of α -Fe₂O₃/epoxy nanocomposites. Epoxy

is a brittle material because it fails in tension at relatively low values of strain. In Fig. 5, the stress-strain curves which remain straight initially represent the elastic region, where the stress and strain are directly proportional. The elastic modulus of the material was measured from the slope of 0.1 to 0.25% tensile strain. Fig. 6 demonstrates the measured tensile properties of α -Fe₂O₃/epoxy nanocomposites. It can be seen that the presence of α -Fe₂O₃ nanoparticles enhanced the tensile stress-strain behavior of the epoxy polymer. Nanocomposites show higher tensile modulus. The increase in modulus is expected because the modulus of α -Fe₂O₃ nanoparticles is about 359 GPa.



Fig. 5 Stress-strain curve of α-Fe₂O₃/epoxy nanocomposites.

The incorporation of α -Fe₂O₃ nanoparticles into epoxy matrix decreased the tensile strength of the nanocomposites because epoxy resin and α -Fe₂O₃ nanoparticles both are brittle materials. Sometimes, agglomeration of nanoparticles inside the polymer matrices becomes responsible for decreasing the tensile strength. This implies that the interfacial bonding between matrix and particle is not strong enough to bear large mechanical stress, as because of inhomogeneous dispersion of nanoparticles. The presence of highly stiff α -Fe2O3 nanoparticles in the polymer matrix is responsible for lowering the elastic modulus and elongation of the polymer [37].

Table 1 Flexural properties of neat epoxy and α -Fe₂O₃/epoxy nanocomposites

Materials	Flexural Strength (MPa)	Strain at Break (%)	Energy (Joule)
Neat epoxy	84.50	1.735	0.0601
0.5% α-Fe ₂ O ₃ /epoxy	76.50	2.127	0.0633
1.0% α-Fe ₂ O ₃ /epoxy	64.50	2.279	0.0338
2.5% α-Fe ₂ O ₃ /epoxy	59.30	1.563	0.0236
5.0% α-Fe ₂ O ₃ /epoxy	53.00	1.850	0.0293

3.6 Flexural Properties Analysis

The three-point flexural test was carried out to determine the flexural properties of α -Fe₂O₃/epoxy nanocomposites, whose force-extension curves are shown in Fig. 7. The neat epoxy, 0.5, 1.0, 2.5, and 5.0 wt% of α -Fe₂O₃/epoxy nanocomposites exhibit

84.5, 76.5, 64.5, 59.3 and 53.0 MPa flexural strength with 1.735, 2.127, 2.279, 1.563 and 1.850% strain at break, respectively which are illustrated in Table 1. From Table 1 we can see that, the addition of α -Fe₂O₃ nanoparticles into the epoxy matrix gradually reduced the flexural strength of the nanocomposites, the reason is due to the compressive characteristics of epoxy resin and α -Fe₂O₃ nanoparticles. The addition of filler is not much effective in flexural characteristics of the matrix but it may increase in the case of laminates with filler matrix [38].





Wt% of α -Fe₂O₃ Nanoparticles







Fig. 7 Force-extension curves of α-Fe₂O₃/epoxy nanocomposites



Fig. 8 Vickers hardness number of neat epoxy and α -Fe₂O₃/epoxy nanocomposites.

3.7 Hardness Analysis

Hardness is the ability of a material to resist plastic deformation, usually by penetration. However, it may also refer to the resistance to bending, scratching, abrasion or cutting. The hardness of neat epoxy, 0.5, 1.0, 2.5, and 5.0 wt% of α -Fe₂O₃/epoxy nanocomposites was measured by Vickers's microhardness tester. These tests were performed at three different loads 98.07, 245.2, and 490.3 mN, respectively, and the results are shown in Fig. 8. The measured values of hardness increased considerably for α -Fe₂O₃/epoxy nanocomposites due to the addition of stiff nanoparticles in the polymer matrix. The successful interaction between nanoparticles and polymer matrix helped to transfer the applied load from matrix to nanoparticles. Thus, the applied load became suppressed by the stiff nanoparticles and the hardness value increased in the composites compared to that of the neat epoxy matrix. In addition incorporation of α-Fe₂O₃ nanoparticles into epoxy resist the movement of dislocation within the structure of the epoxy matrix, increases hardness.

3.8 TG Analysis

Fig. 9 shows the TG curve of α -Fe₂O₃ nanoparticles, neat epoxy, and 5.0% α -Fe₂O₃/epoxy nanocomposite, respectively. The decomposition process consists of three regions. They were 20-300 °C, 300-500 °C, and 500-600 °C, respectively. The first weight loss indicates the evaporation of absorbed water due to the initial breakdown of the complex and spontaneous combustion. H₂O and CO₂ provide an oxidizing environment for the combustion of the organic components [39], citrate ions in the gel cause spontaneous combustion. The second weight-loss indicates the dehydration of the O-H group in the α -Fe₂O₃ structure and epoxy that lead to two degradation systems involving both inter and intra-molecular transfer reaction, the oxidation of complexes, and formation of semi-organic carbon metal/metal oxide [40]-[42].



Fig. 9 TGA curve of α -Fe₂O₃ nanoparticles, neat epoxy and 5.0% α -Fe₂O₃/epoxy nanocomposite



Fig. 10 Absorbance vs wavelength curve of α-Fe₂O₃/epoxy nanocomposites

The third weight loss indicates the formation of the corresponding metal oxide phase. Above 600 ^oC there is no weight loss i.e. the TGA curve is steady, exhibiting the absolute volatility of water, organic compounds, citrates in the composites, the completion of crystallization route, and the immediate formation of pure materials.

3.9 UV-Vis Spectroscopy Analysis

UV-Vis spectroscopy is used to determine the optical band gap energy of crystalline and amorphous materials. In this method, electron excitation from the valance band to the conduction band, is used to verify the character and value of the optical band gap. UV-visible spectra of fabricated specimens were measured in the 190-1100 nm range, (Fig. 10). The spectrum of neat epoxy shows a single absorption peak at 526 nm, which represents the polaron/bipolaron transition. On the other hand, spectra of α -Fe₂O₃/epoxy nanocomposites show several peaks within the entire range in shells increase the absorption cross-section of the nanocomposite and thus enhance plasma-exciton interactions [43]-[45]. The optical band gap is determined using the following relationship [46]:

$$\alpha h v^{\frac{1}{n}} = A(hv - E_q) \tag{1}$$

For direct band gap materials this equation becomes-

$$\alpha h v = A(h v - E_a)^2 \tag{2}$$

where α is the absorption coefficient, A is a constant, E_g is the optical band gap of the material and the exponent n depends on the nature of electronic transition, it is equal to 1/2 for direct allowed, 3/2 for direct forbidden transitions, and 2 for indirect allowed transition. An extrapolation of the linear region of a plot of the graph of $(\alpha h \upsilon)^2$ on the y-axis versus photon energy (h υ) on the x-axis, gives the value of the optical band gap, E_g [47]. The optical band gap is calculated and shown in Fig. 11. From Fig. 10, we can see that, the absorbance of α -Fe₂O₃/epoxy nanocomposites increased with increasing the α -Fe₂O₃ content. The increased light absorption phenomena can be attributed to the well dispersion and successful interaction of nanoparticles inside the polymer matrix.

Conversely, from Fig. 11, we can see that, the optical band gap of neat epoxy, 0.5, 1.0, 2.5, and 5.0 wt% of α - Fe₂O₃/epoxy nanocomposites were 3.2, 2.8, 2.4, 1.8, and 1.4 eV, respectively. This decrease of E_g can be attributed to the formation of complex due to interaction between nanoparticles and polymer matrix. In addition, the increase of density of defects i.e. particle clusters leads to the expansion of valance band inside the forbidden gap of polymeric system. Therefore, band tailing occurred and as a consequence shrinkage of Eg was happened [48].

3.10 DC Resistivity Analysis

Fig. 12 shows the I-V curves of neat epoxy, 0.5, 1.0, 2.5 and 5.0 wt% of α -Fe₂O₃/epoxy nanocomposites, where all the tests were performed at room temperature. This figure indicates that 5.0 % α -Fe₂O₃ nanoparticles containing epoxy nanocomposite have the higher value of dc current, I (about 27.342 nA) at 50 volts, whereas neat epoxy shows the minimum value of dc current, I (about 18.741 pA) at 10 volts. On the other hand, Fig. 13 shows the variation of measured dc resistivity (ρ) of neat epoxy, 0.5, 1.0, 2.5 and 5.0 wt% of α -Fe₂O₃/epoxy nanocomposites. This figure illustrates that neat epoxy exhibits the highest value of dc resistivity, ρ (about 3.017 TΩmm) because epoxy is an excellent electrically insulating material, whereas 2.5% α -Fe₂O₃/epoxy nanocomposite exhibits the lowest value of dc resistivity, ρ (about 0.923 TΩmm).



Fig. 11 Optical band gap of α-Fe₂O₃/epoxy nanocomposites

By increasing the α -Fe₂O₃ content into epoxy, the dc resistivity of the nanocomposite sheets decreased gradually due to the formation of polarons in the both epoxy and α -Fe₂O₃ molecules after applying voltage [49]. By increasing α -Fe₂O₃

content, the dc resistivity changes slightly, which attributed to saturation of charge carriers.

However, $1.0\% \alpha$ -Fe₂O₃/epoxy nanocomposite exhibited a little inconsistency of dc resistivity may be due to the non-

uniform dispersion and agglomeration of α -Fe₂O₃ nanoparticles into the epoxy matrix. Moreover, this happened due to the dispersion of higher amount of nanoparticles than the critical volume fraction in the polymer matrix.



Fig. 12 I-V curves of α -Fe₂O₃/epoxy nanocomposites



Fig. 13 Effect of α -Fe₂O₃ nanoparticles on the dc resistivity of α -Fe₂O₃/epoxy nanocomposites

4 Conclusions

In this study, we synthesized α -Fe₂O₃ nanoparticles by solgel process which further dispersed into the epoxy matrix to fabricate nanocomposites. The chemical, mechanical, electrical, optical and thermal properties of the fabricated polymer nanocomposites were evaluated. The XRD and SEM confirmed the formation of nanoparticles. FTIR analysis ensured the presence of different functional groups into the nanomaterials. Using VSM measurement, the saturation magnetization (M_s) , coercivity (H_c) and remnant magnetization (M_r) of α -Fe₂O₃ nanoparticles were found to be 337.137×10^{-3} emu, 33.312 Oe and 28.90×10^{-3} emu, respectively. Incorporation of α -Fe₂O₃ nanoparticles into epoxy matrix gradually decreased tensile strength, elongation, flexural strength, optical band gap energy and dc resistivity of α-Fe₂O₃/epoxy nanocomposites, however, increased the young modulus, surface hardness and thermal stability of α-Fe₂O₃/epoxy nanocomposites. The fabricated nanocomposites can be used to produce various products in medical, construction, automotive, etc. sectors with better properties based on the obtained results.

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